PATENT SPECIFICATION

637.019



Date of Application and filing Complete Specification: July 29, 1947.

No. 20504/47.

Application made in United States of America on Sept. 12, 1944.

Complete Specification Published: May 10, 1950.

(Under Rule 17A of the Patents Rules 1939-47, the proviso to Section 91 (4) of the Patents & Designs Acts, 1907 to 1946 became operative on July 29, 1947.

Index at acceptance:—Classes 69(i), R; and 135, H4, P(1b:7), P9a(3:6), P16(b:c:e3), P(18:23), P24(f:kx).

COMPLETE SPECIFICATION

Improvements in or relating to a Flow Meter

We, Penn Industrial Instrument Corporation, a corporation organized under the laws of the State of Pennsylvania, United States of America, of 3116 N. 17th Street, City of Philadelphia, Zone 32, State of Pennsylvania, United States of America, do hereby declare the nature of this invention and in what manner the same is to be performed, to be particularly described and ascertained in and by the following state-

This invention relates to the type of flow metering device in which a movable 15 obstruction attains a position establishing a condition of a variable orifice such that the position is indicative of a fluid flow. A typical device of this type is the rotameter in which a float moving within a 20 tapered tube provides a variable area for the passage of fluid and assumes a position which is dependent upon the rate of fluid flow. The invention is particularly concerned with the provision of means 25 for indicating remotely the position of the obstruction, such as said float, and, hence, for indicating remotely the rate of flow.

The general object of the invention is 30 the provision of a pneumatic type of remote indicator capable of accurately responding to variations in the flow rate, and in particular independently of temperature changes. This general object 35 and other objects of the invention, particularly relating to details, will become apparent from the following description, read in conjunction with the accompanying drawings, in which:

O Figure 1 is a longitudinal sectional view of a rotameter with which are associated the remote indicating devices;

Figure 2 is a perspective view partially in section showing one form of float;

Figure 3 is a similar view showing an 45 alternative form of float;

Figure 4 is a diagram showing a remote indicating system and, in particular, showing a relay in section;

Figure 5 is a fragmentary diagram- 50 matic view showing an alternative relay arrangement for giving remote indications of the flow:

tions of the flow;
Figure 6 is a diagram of an alternative indicating system having certain advan- 55 tages, particularly independence of a variable supply pressure;

Figure 7 is a diagram of still another system embodying the invention; and

Figures 8 and 9 illustrate in diagram-60 matic sections two types of variable resistances which may be used in conjunction with the invention.

Referring first to Figure 1, the rotameter shown therein, as typical of a 65 meter to which the invention is applicable, comprises a tube 2 having a tapered interior, which tube is of a type commonly used in rotameters. In the event it is desired that the rotameter readings 70 should be observed locally as well as remotely, the tube may be transparent and provided with suitable graduations against which the positions of the float may be read to give indications of rate 75 of flow. The ends of the tube are engaged in fittings 4 and 6 provided with the respective inlet and outlet openings 8 and 10, through which fluid may be admitted for flow through the tube 2. 80 Suitable packing 12 and 14 is associated with the fittings 4 and 6, the tube, and the protective casing 16, the construction in these respects being substantially conventional and requiring no detailed 85 description.

A float 20 which may be of conventional exterior form is, as contrasted with

prior types of rotameters, provided with a somewhat enlarged bore serving to receive the fixed cylindrical tube 22 of brass or other non-magnetic material. The float 20 has a sliding fit on this tube.

The float 20 has a sliding fit on this tube. In the interior of the tube 22 is a tapered tube 24 preferably of glass inasmuch as such a tube may be provided with an accurately shaped bore which, in this interior is the read being appeared as in

10 stance, is tapered, being enlarged as indicated at its upper end as compared with its lower end. The upper end of this tube is vented to the atmosphere at 26. It may be positioned against a lower seat

15 in the tube 22 by means of a light spring 27. Within the tube 24 is a steel ball 28 which is arranged to follow the float by reason of the provision of magnets within the float as will be hereafter des-

O cribed in greater detail. Adjacent its lower end, the tube 24 is provided with a seat 30 to catch the ball and retain it when the float drops beyond its useful

operating range.

For the purpose of providing remote indications various air connections are present including a connection 32 in free communication with the space 34 within the lower end of the tube 22 which com-30 municates with the lower end of the tapered tube 24. A supply of air to the lower end of tube 24 is effected through the connection 40 leading to a capillary tube 42 which provides a resistance to 35 flow of air and which delivers the air into a space 36 in a thimble 38 threaded into the fitting 4, which space 36 communicates through a passage 44 with the space 34. The capillary tube 42, it will be 40 noted, is located in the lower fitting 4. As a result of this construction it is at all times substantially at the temperature of the ball 28 and tube 24. Thus both flow resistances are subject to the same 45 temperature variations and compensation is thereby effected.

As illustrated in Figure 2, the float 20 may be provided with a pair of magnets 45 and 46 positioned with their opposite poles across the bore in the float from each other. These magnets will pick up the ball 28 as the float moves and will always maintain it in a position accurately corresponding to the position of the

55 float.

An alternative arrangement of magnets is indicated in Figure 3 in which a float 20¹ is provided with arcuate magnets indicated at 48 and 50 with their 60 like poles adjacent to each other, thereby providing a strong magnetic field extending across the bore and so carrying the ball 28 as the float moves. The ball is thus positioned so as to have 65 varying clearance with the tapered walls

of the tube 24 affording a variable resistance which is related to the float position and, therefore, to the rate of flow

through the meter.

The remote indicating devices are 70 essentially measuring devices for the resistance to flow which appear at the location of the ball 28. One system for accomplishing this is indicated in Figure 4. In this figure, the matter to the left 75 of the broken line represents diagrammatically the rotameter just described. Indicated therein in diagrammatic fashion are the ball 28, the tapered tube 24 in which the ball moves, and the connections 32, 34, 40, and 44, with the resistance afforded by the capillary tube 42 being indicated diagrammatically.

For the purpose of giving indications of the very slight changes in resistance to 8 air flow produced at the ball 28, there is provided a relay indicated generally at 52. This is provided with a chamber 54 closed by a flexible diaphragm 56 and communicating with the connection 32. 90 (The relay is also provided with an upper diaphragm chamber which, in the pre-sent application, is not used, though such a chamber is used in a modification later to be described). The diaphragm 56, 95 through an abutment 58, acts upon a pivoted arm 60 which, through a flexible wire 62, is arranged to move a connected pair of pistons 64 and 66 in a cylinder 68. The connection 40 is joined 100 to an opening 70 which communicates with a port 72 slightly less in diameter than the length of the face of the piston 66 which has only a slight movement to open the port 72 to either the space above 10 or the space below the piston. A port 74 joins the space between the pistons 64 and 66 with a passage 76 to which a supply of air under pressure is applied through the line 78. The space below 11 the piston 66 is vented to the atmosphere through openings indicated at 80 and 82. A pressure gauge 84 is connected to the line 40 and serves to indicate a pressure P which will be a function of the resist- 11! ance at the ball 28 and, consequently, of the rate of flow through the meter. The following will make clear the relationship of the pressure P to the resistance to an air flow occasioned by the ball 28. 120

Suppose in the modification of Figure 4, the variable resistance R is provided by the ball, which resistance is a function of the position of the float. By the diaphragm action the pressure between 125 resistances R_o and R is maintained constant at some value P_o fixed by the downward pressure on the diaphragm 56. The action of the valve will be to provide a pressure P at the gauge, the 136

637,019

relationship of which to R may be determined as follows:

The flow I of air through R and R_o is the same, save for minute quantities entering the diaphragm chamber 54 which is of very small volume. Therefore:

 $P - P_o = R_o I$ $P_o = RI$

10 Elimination of I gives:

$$P = P_o \left(1 + \frac{R_o}{R} \right),$$

the functional relationship between P and R. P is therefore a function of the float position and may be calibrated to give direct readings of fluid flow.

It will be noted that the supply pressure P_s does not enter into the above so that it need not be regulated except to the extent that it must be greater than 20 P.

It will be evident from the above that by a proper choice of R_o and P_o the pressures appearing on the gauge may be very much magnified over the pressure existing at P_o, which pressure will normally be quite small inasmuch as the rate of air flow is desirably kept low. While the pressure P_o is small, it can be made to act upon a quite large diaphragm at 56 so as to be capable of affording positive control of the valve.

While the pressure at P_o is held con-

while the pressure at Po is held constant in the modification of Figure 4, that condition need not be established, 35 but certain alternative forms of indicators of the resistance R may be provided, one of which is indicated diagrammatically in Figure 5 in which it will be understood that the connections indicated 40 at 32¹ and 40¹ are connected to 32 and 40, respectively, at the position of the broken line. The connection 32¹ communicates with the chamber 86 closed by a diaphragm 88. An upper chamber 90 is closed by a diaphragm 92 which acts in opposition to the diaphragm 88 upon a lever 94, the construction being somewhat similar to that previously indicated at 52. The lever 94 operates joined 50 pistons 96 and 98 in a cylinder 100.

The air pressure supply line indicated at 102 feeds air to a constant pressure regulating valve 104 which delivers air at constant pressure to the line 106 which 55 connects with the line 40¹. A connection 108 from the line 40¹, 106 communicates with a port opening to the space between the pistons 96 and 98.

A port 110 having a diameter slightly 60 less than the axial extent of the piston

96 is normally overlapped by this piston, movements of which is an upward direction furnish communication between the line 108 and the port 110 and movements of which in a downward direction 65 vent the port 110 to the atmosphere. A line 112 connected to the port 110 leads to a pressure gauge 114 serving as an indicator for the system. Two resistances 116 and 118 arranged in series serve to 70 vent the line 112 to the atmosphere. Between these resistances there is the connection 120 to the upper diaphragm chamber 92.

In the case of the modification of 75 Figure 5, R and R_o may be considered to be as before, pressure P_o existing between R and R_o and applied to the lower diaphragm chamber. P_s is the supply pressure, in this case regulated, since, as will be seen hereafter, it enters into the calibration of the system. Resistances R₁ and R₂ exist as indicated, as do also pressures P and P₁. Let the flows through R_o and R and through R₁ and R₂ be, respectively, I₁ and I₂. Let F be a downward force on the lower diaphragm in terms of effective force per unit area thereof.

Then: 90
$$P_{s} - P_{o} = R_{o}I_{1}$$

$$P_{o} = RI_{1}$$

$$P_{-P_{1}} = R_{1}I_{2}$$

$$P_{1} = R_{2}I_{2}$$

$$P_{1} + F = P_{o}$$
 95

Elimination of I_1 , I_2 , P_0 , and P_1 from these gives:

$$P = \left(1 + \frac{R_1}{R_2}\right) \left(P_8 - \frac{1}{\left(1 + \frac{R_0}{R}\right)} - F\right)$$

The force F referred to in the foregoing may be applied by a weight or spring, and it will be evident that it serves to change the range of pressure P corresponding to a particular range of variation of resistance R. A further possibility of adjustment, it will be 105 noted, is involved in the setting of the valve 104 to control a particular constant pressure P_s . If a spring is used to supply the force F there will be a slight deviation of actual conditions from what 110 is represented by the foregoing expression for P, the deviation depending upon the departure of the actual relay from an ideal one in which the pilot valve has no

motion. Actually F will be variable with the motion of the pilot valve necessary to open the top or bottom of the port at 110. Such motion may, however, 5 be very small.

In the modification shown in Figure 5 the flow of air past the ball is nearly constant, the pressure drop across R being negligible in comparison with that

10 across Ro.

As will be seen from the foregoing examples, a remote indication of the position of the float of the rotameter is made possible. The particular lines connected to a remote position are, of course, subject to variation. If the relay of either type is located remote from the meter, two lines may be run to the relay and the pressure gauge located thereat.

20 On the other hand, the pressure gauge

On the other hand, the pressure gauge may be at a remote position with the rotameter and relay adjacent each other. It will be evident that essentially what is involved is a very substantial magnifica-

5 tion of the pressure drop which exists across the ball 28. By magnification, it is not meant that this magnification is linear, but rather that a large pressure difference can be made to appear at a gauge and will be a function of the resistance presented at the ball 28.

While the description has indicated the ultimate application of the magnified pressure to a pressure gauge, it will be system may be utilized for control purposes in conventional fashions, controlling, for example, a valve regulating the flow which takes place through the rotameter with the objective of maintaining such flow constant, or, alternatively, such pressure may be applied for controlling the application of heat to a system which also involves flow and wherein a quantity of heat added is some function of a rate of flow. Still another application would be the control of some pressure in accordance with a rate of flow. It will thus be evident that the

50 invention is of very broad applicability.

It will also be noted that this invention is not limited to a rotameter which has been described merely by way of a typical application of the invention to 55 which it is very well adapted. Any movable obstruction or element capable of carrying a member such as the ball 28 could have its position indicated by the means described. In various applications the ball may be replaced by a rod moving in a tapered or uniform diameter tube, as at 300 in Figure 8 or at 302 in Figure 9, respectively. The sole limitation on structural possibilities is 65 that the control of the variable resist-

ance should not entail execution of any such force as will react on a float or other moving member to displace it to a substantial degree from a position which it would normally assume under the 70 action of fluid flow. By this there is, of course, meant a variable force. The weight of a ball such as 28 may be merely considered as part of the weight of the float. By the use of an amplify- 75 ing relay system of the type described the forces, exerted by air flow, may be kept so low as not to become disturbing factors.

It was remarked above that the supply pressure does not enter into the operation of the modification in Figure 4 and this is true provided the valve is well balanced and the variations in supply pressure are not too great causing a 85 degree of unbalance. In order to avoid any possible disturbing effects due to supply pressure fluctuations and additionally to secure other advantages such as further elimination of friction, it is desirable under some circumstances to provide a more elaborate responsive device such as one of those illustrated in

Figures 6 and 7.

Referring first to Figure 6, there is 95 indicated at 130 a tapered tube in which moves a ball 132 to provide a movable obstruction giving rise to a variable resistance to the flow of air. As indicated above this is merely an example of a 100 variable resitance member which may take other forms. The elements illustrated in Figure 6 produce a pressure responsive to the value of the resistance appearing at 132. A supply 105 ae 134 feeds air to the line A resistance 136 is interposed between the supply line and an orifice or nozzle 138 closely adjacent to which is an end of a lever 140 having an adjust- 110 able substantially fixed force applied to it at 142. A chamber 144 closed by a diaphragm 146 is connected to the lower end of the tube 130 by a line 148. This diaphragm is mechanically connected to 115 the lever 140. A line 150 from the nozzle 138 communicates with a chamber 152 closed by a large diaphragm 154 and a smaller diaphragm 156 as indicated, both of which are mechanically con- 120 nected to the lever 140. The space 158 above the diaphragm 154 is open to the atmosphere. A line 160 leads from the nozzle 138 to a chamber 162 provided with a large upper diaphragm 164 and 125 a smaller diaphragm 166, both of which are connected to a lever 168 which controls valve 170 provided with seats in a valve housing 172. This valve is merely diagrammed in Figure 6 and may take 130 either the form of a valve member moving between the seats as indicated or of a slide valve of one of the types previously described. The operation of this pilot valve is to control the pressure in an outlet line 176, there being a connection between the valve casing and the source of air at 174. The output of the pilot valve is connected through line 178 and variable resistance 180 with the lower end of tube 130. The resistance 180 may be of the type described in connection with Figure 1 built into a rotameter or other flow meter.

15 Two fixed resistances 182 and 184 are provided between 176 and the atmosphere. The junction between them is connected to a chamber 188, the lower wall of which is provided by the diaphragm 164 previously described. Chamber 188 is connected through a passage 190 and an adjustable resistor 192 with a chamber 194 closed by a diaphragm 196 connected to the lever 168. The upper side of the diaphragm 196 is open to the atmosphere. A spring 198 may be adjusted to provide a suitable force on the lever 168. A gauge 200 is connected to 176 to give pressure indications corresponding to the position of the obstruction 132. This gauge may be calibrated directly in terms of the flow through the meter.

Pressures and resistances Po, R and Ro corresponding to those of Figure 4 are designated by the same reference characters and the outlet pressure P is related to the constant pressure P₁ and to the resistances R and Ro in the identical 40 fashion given above for the relation of P to Po in the modification of Figure 4. The pressure P₁ is a constant function of the forces F₁ and F₂ applied to the levers. Under equilibrium conditions Po

Under conditions of a change of resistance R transient relations are set up which involve a floating action. Assume, for example, an increase in the resistance R. The pressure Po immediately rises and the baffle provided by the lever 140 moves slightly away from the nozzle 138 with consequent decrease of the nozzle pressure Po. This decrease acting in the chamber 152 equalizes the increase of pressure Po with the result

that the nozzle pressure always changes by an amount which is directly proportional to the change in the pressure Po. 60 The pressure P1 is applied to chamber 162 resulting in a corresponding decrease in the output pressure P. By reason of the consequently reduced flow through resistance 180 the pressure Po is 65 then reduced toward its initial value.

Without the provision of anything further it would be evident that the pressure Po would never be brought back exactly to its initial value by this proportional action alone. However, by the 70 action of chamber 188 and 194 and the connecting resistance 192, the pressure Po is restored to its initial value. This occurs because by reason of the reduction of pressure P, there is a reduction of the 75 pressure P₂ between the resistances 182 and 184 and in the chamber 188. Flow of air accordingly takes place from the chamber 194 to the chamber 188 through the resistance 192 giving a floating action 80 which continues until the pressure Po has been restored to its initial value and the nozzle pressure P_1 is also at its initial value. Finally the pressures P_2 and P_3 are once again equal but at a lower value 85than that existing before the assumed

change in resistance R. The modification illustrated in Figure 7 is essentially identical with that involved in Figure 6 with the exception 90 that the floating action is introduced into the first relay instead of the second. In Figure 7, the tube 202 and ball 204 provide a variable resistance as before. The supply line 206 supplies through 95 fixed resistance 208 the nozzle 210 with which cooperates the lever 212 acting as a baffle and properly biased by the force exerted by the adjustable spring 214. A connection 224 joins the lower end of the 100 tube 202 with a chamber 226 provided with a diaphragm 228 connected to the lever 212. Below the diaphragm 228 is a second chamber 230 which is closed by a small diaphragm 231 also connected to 105 the lever 212. The chamber 230 is connected to the nozzle 210 through the resistance 260.

The nozzle 210 is connected through tube 232 to a chamber 234 closed by a 110 diaphragm 236 which acts upon the lever 238 biased by the adjustable force exerted by a spring 240 and arranged to actuate a valve 242 of the type previously described. The valve is supplied with 115 air from line 206 through connection 244 and delivers air at controlled pressure to the line 246 and the pressure gauge 248. Resistances 250 and 252 in series vent the line 246 to the atmosphere. Connec-120 tion 254 joins the junction of the resistance 250 to a chamber 256, the diaphragm 258 enclosing which is connected to the lever 238.

A chamber 262 closed by a large dia- 125 phragm 264 and a small diaphragm 266 is illustrated, both of which are connected to the lever 212, communicates through passage 270 with the connection 232. The space 268 below the diaphragm 130

264 is vented to the atmosphere.

The action of the system of Figure 7 is, as stated, that of Figure 6 and need not be described in detail. A floating action exists at the upper relay due to the presence of the resistance 260. To increase the time constant of this the volume of the chamber 230 may be increased by the addition of an air chamber 272 connected to it

Additionally, there exists in this modification an amplification by reason of the effective area of the diaphragm closing chamber 226 in relation to the effective area of the diaphragms enclosing chamber 262 which area is the difference between the areas of diaphragms 264 and 266. This area amplification is desirable inasmuch as the drop of pressure across 20 the ball 204 should be kept to the order

of one inch of water. For practical purposes it is desirable to deliver an output pressure ranging up to fifteen pounds per square inch. Overall pressure amplifica25 tion of the order of five hundred is

required. Imperfections in pilot valve characteristics make it difficult to achieve such a high amplification without serious nonlinearity, and consequently it is desirable to introduce part of the ampli-

fication in one of the relays by the use of the ratio of areas which can readily be made of the order of five. Thus the associated amplification by the arrangement of resistances need not be greater

than about one hundred, an amplification which can be satisfactorily attained. It may be noted that such area amplification is also applicable to the modification shown in Figure 6.

Having now particularly described and ascertained the nature of our said invention and in what manner the same is tobe performed, we declare that what we

45 claim is:—

1. In combination a flow meter comprising a member displaceable in accordance with flow of a fluid, said member being provided with a magnet, an element of magnetic material adapted to 50 be movable with said member forming an obstruction to flow of a second fluid and providing in conjunction with a cooperating element a resistance variable with the position of said member, means 55 providing a flow of the second fluid through said resistance and means for producing a pressure which is a function of the resistance to flow provided by said obstruction, said pressure being in excess 60 of the pressure appearing at said variable resistance.

2. A combination according to claim 1 in which the flow meter member is located in the first mentioned flowing fluid and is displaceable in accordance with flow by drag of the fluid thereon.

3. A combination according to either of claims 1 or 2 in which the flow meter member comprises a float provided with 70 a magnet and arranged to assume a variable position corresponding to a rate of flow through the meter, and in which the cooperating element is a tube of varying internal cross-section in which the 75 element of magnetic material is adapted to be carried by said magnet.

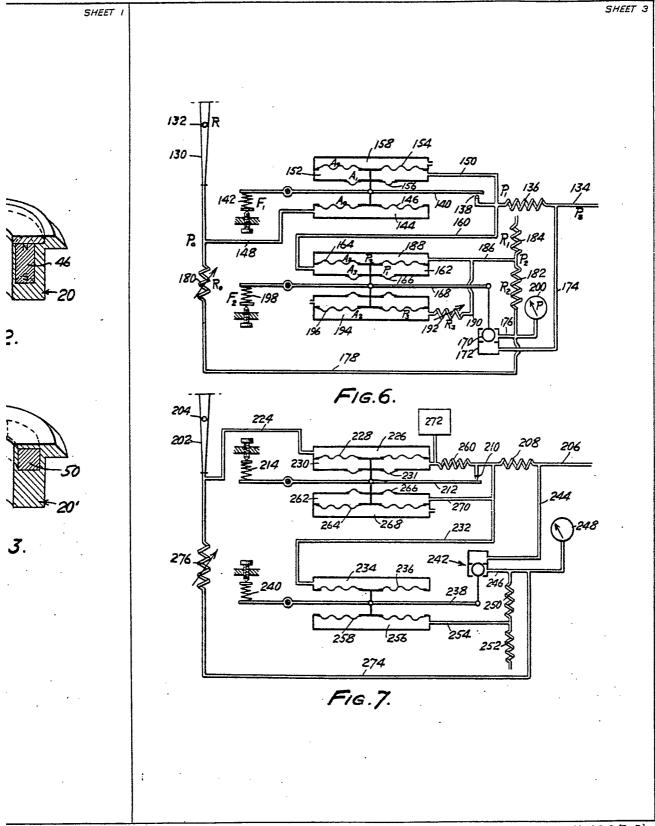
4. A combination according to any of the claims 1 to 3 in which the pressure produced by the pressure producing 80 means varies through a range exceeding the range of pressure appearing at said

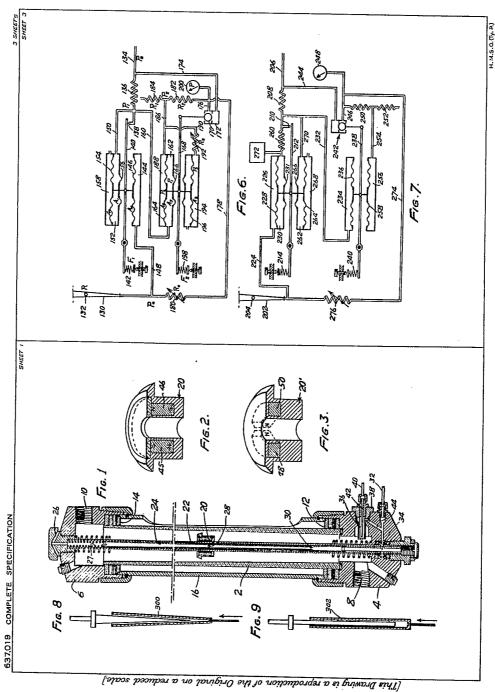
variable resistance.

Dated the 29th day of July, 1947.

HASELTINE, LAKE & CO.,
28, Southampton Buildings,
London, England, and
19/25, West 44th Street,
New York, U.S.A.,
Agents for the Applicants.

Leamington Spa: Printed for His Majesty's Stationery Office, by the Courier Press.—1950. Published at The Patent Office, 25, Southampton Buildings, London, W.C.2, from which copies, price 2s. 0d. each (inland) 2s. 1d. (abroad) may be obtained.





H.M.S.O. (Ty.P.)